



The 3rd Workshop on Reactive Metal Processing

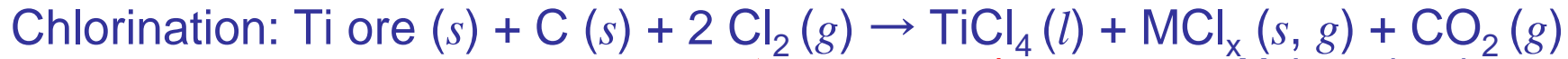
AN ENVIRONMENTALLY-SOUND PROCESS FOR RECYCLING Ti SCRAP COMBINING WITH CHLORIDE WASTES

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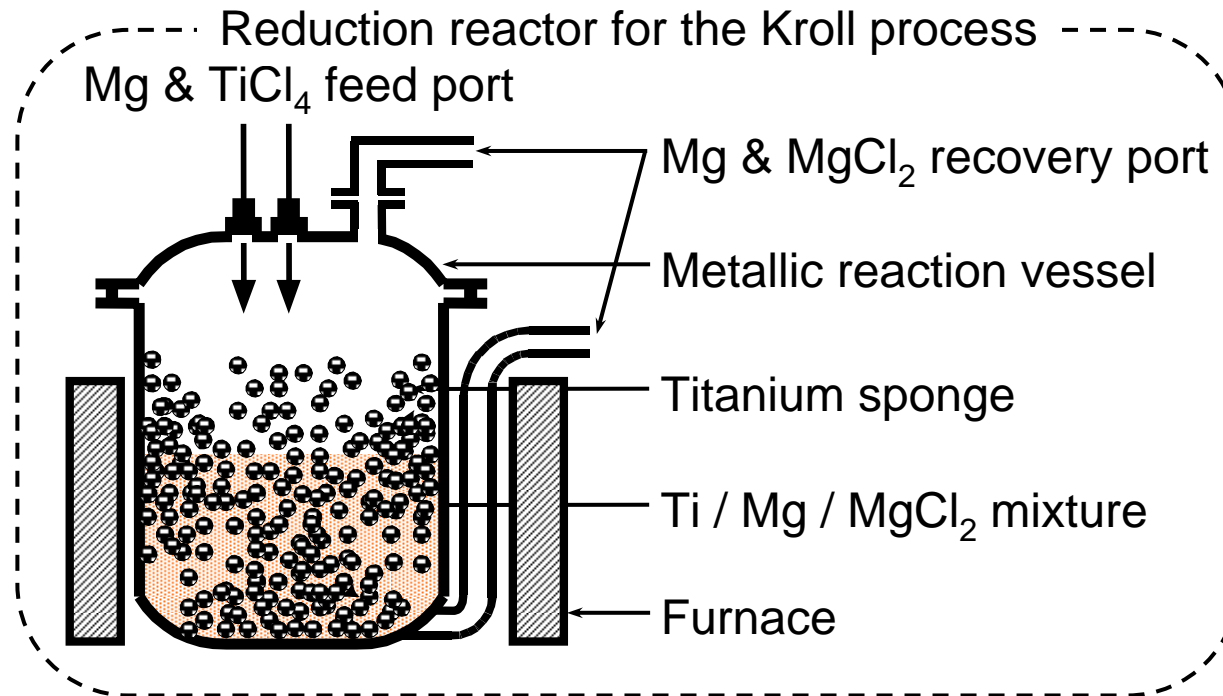
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The Kroll process



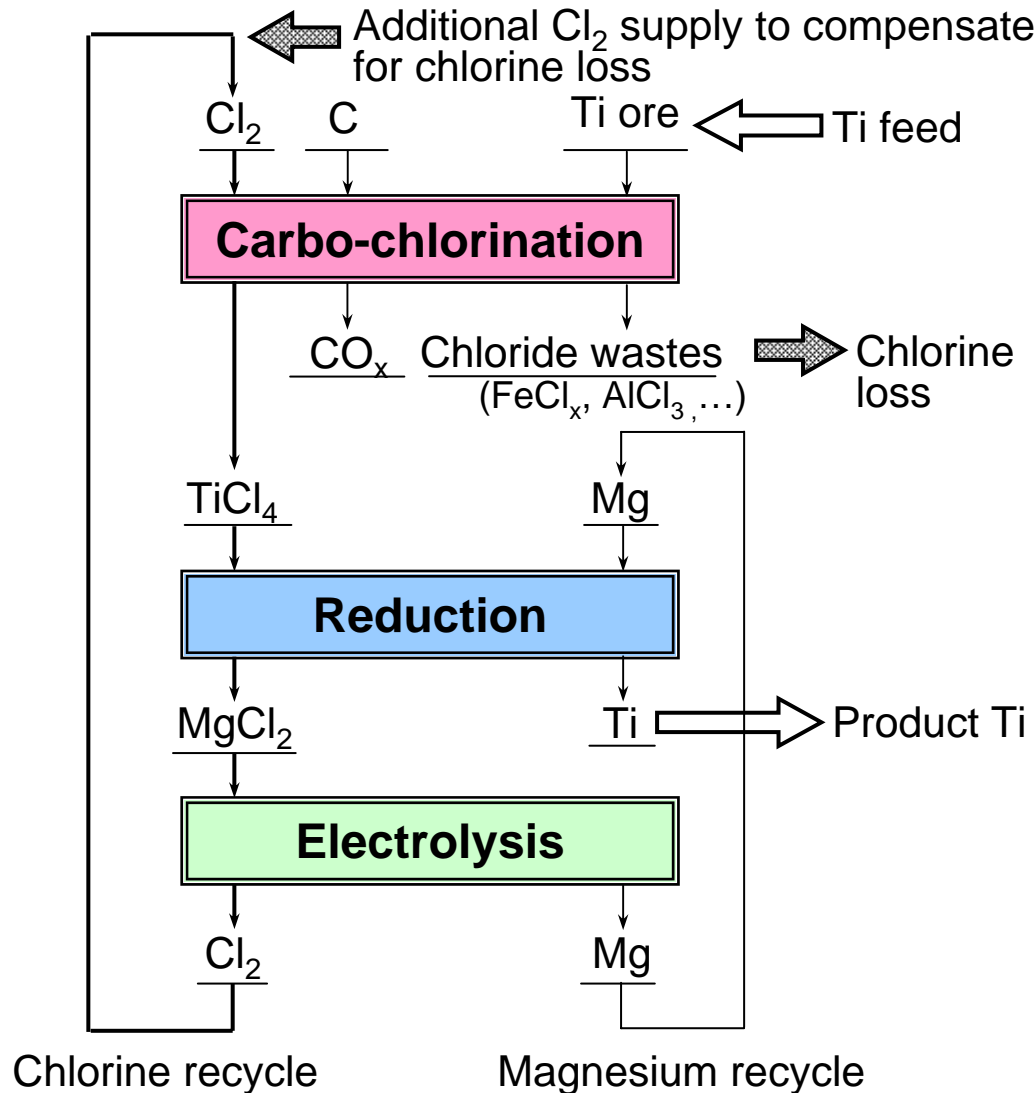
M: Impurity element in the ore



The essential advantage: High-purity Ti available

The critical disadvantage: Low productivity

Chlorine cycle in the Kroll process



Although major portion of chlorine in the Kroll process is recycled, chloride wastes are generated in the Kroll process.

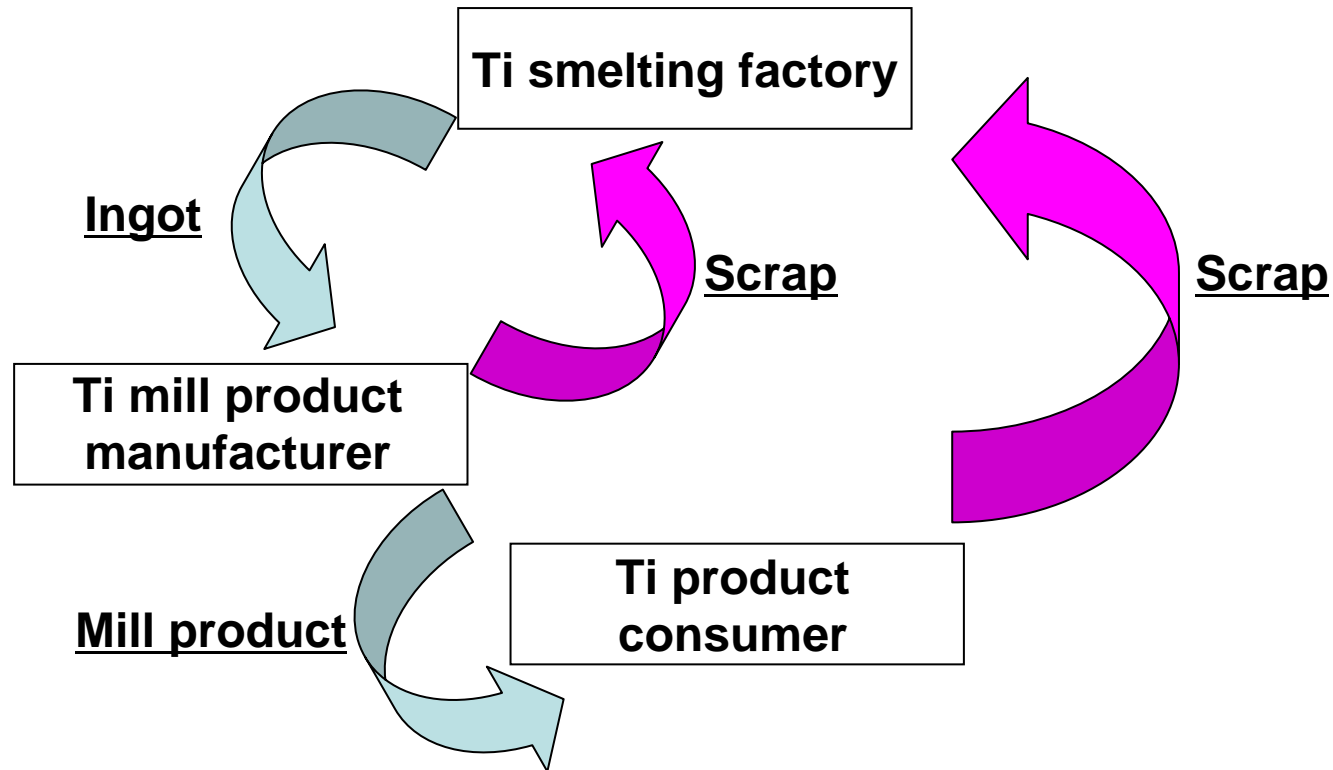


The generation of chloride wastes causes not only chlorine loss but also environmental problems.

Current Ti scrap recycle

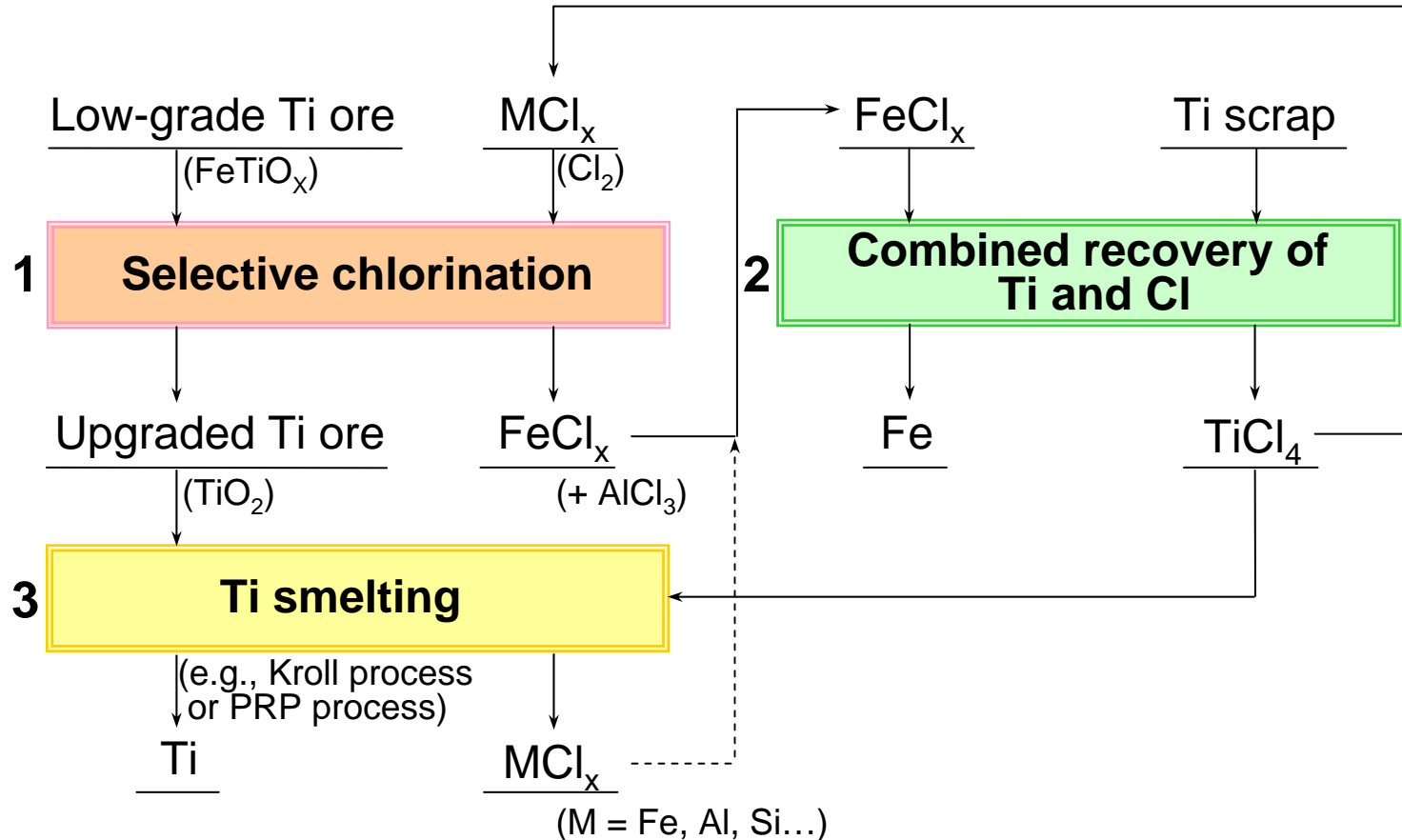
1) Ti scrap is used for producing ferro-alloys for steel making.

2)



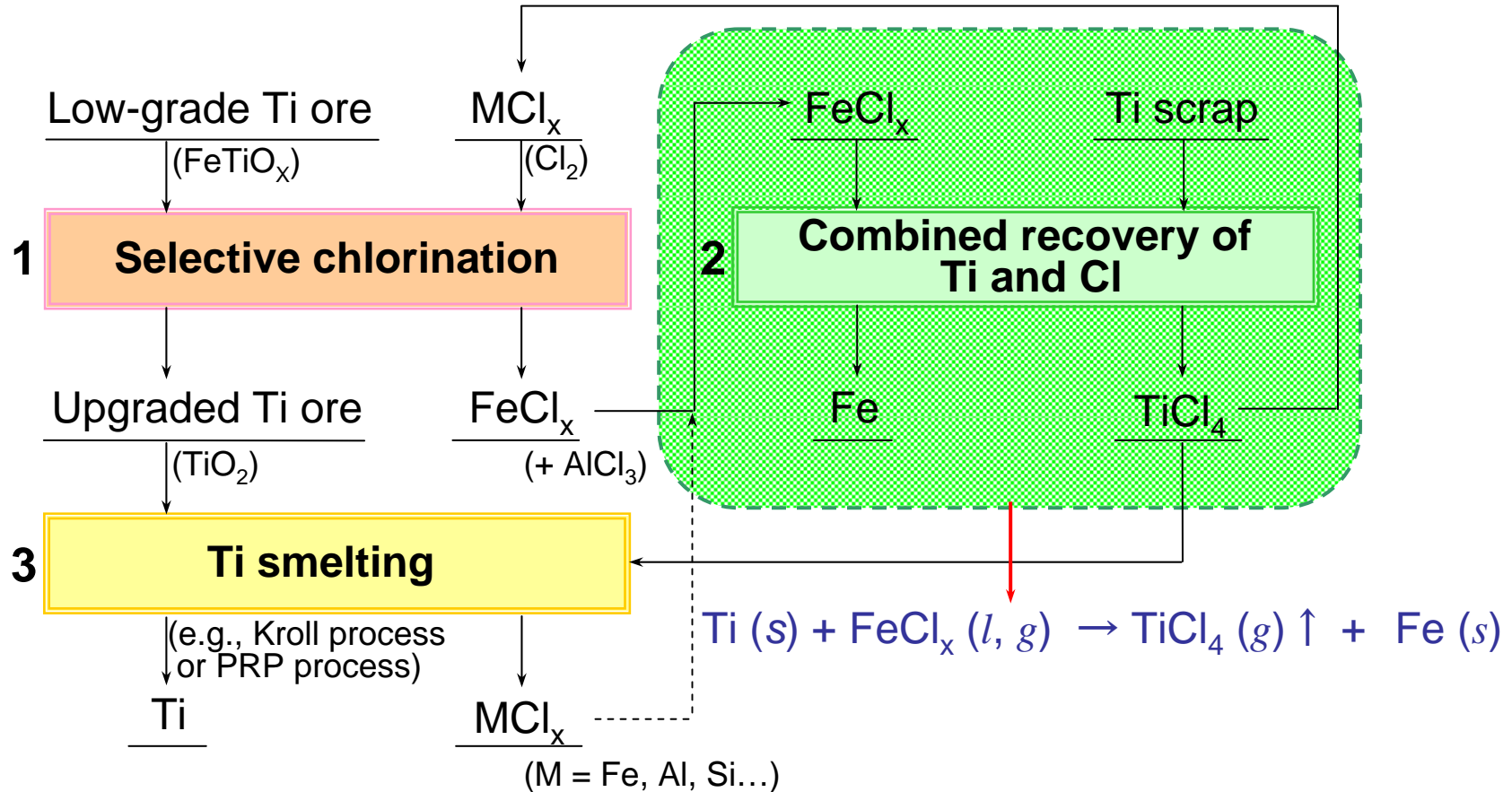
In the future, amount of low-purity Ti scrap will increase, and a new recycling process of Ti scrap is required.

The purpose of this study



A new Ti smelting process combined with iron removal from low-grade Ti ore by selective chlorination and efficient Ti scrap recovery by utilizing chlorine wastes is investigated with the objective of reducing the production cost and decreasing the environmental burden.

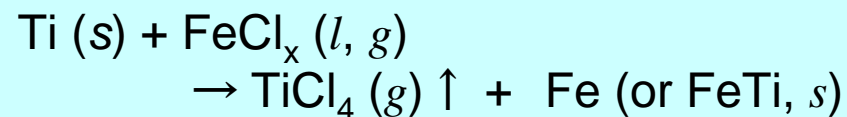
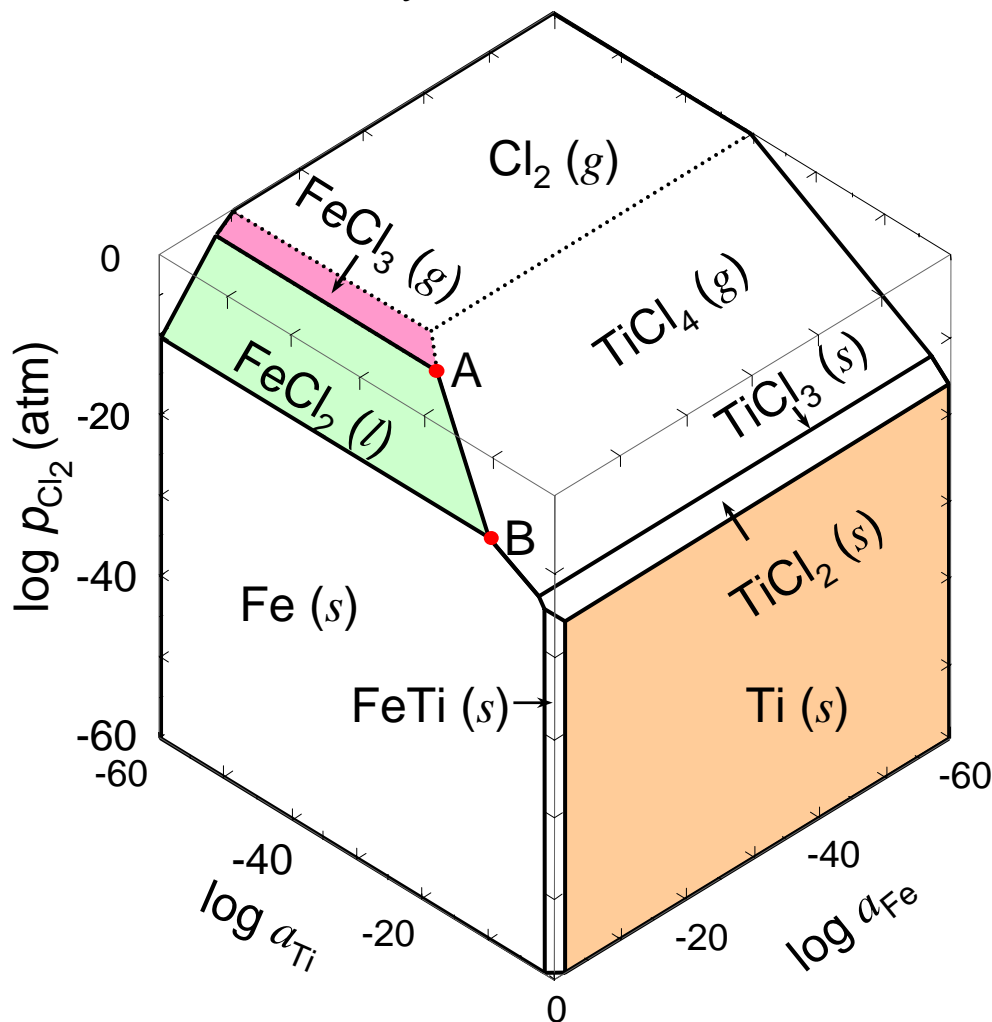
Today's topic



- **Ti metal scrap can be recycled.**
- **Chlorine in the chloride wastes can be efficiently recovered.**
 - **Low-grade Ti ore can be used as the feed material.**
 - **Cost of waste treatment can be reduced.**

Chemical potential diagram for the Fe-Ti-Cl system

Fe-Ti-Cl system, $T = 1100$ K

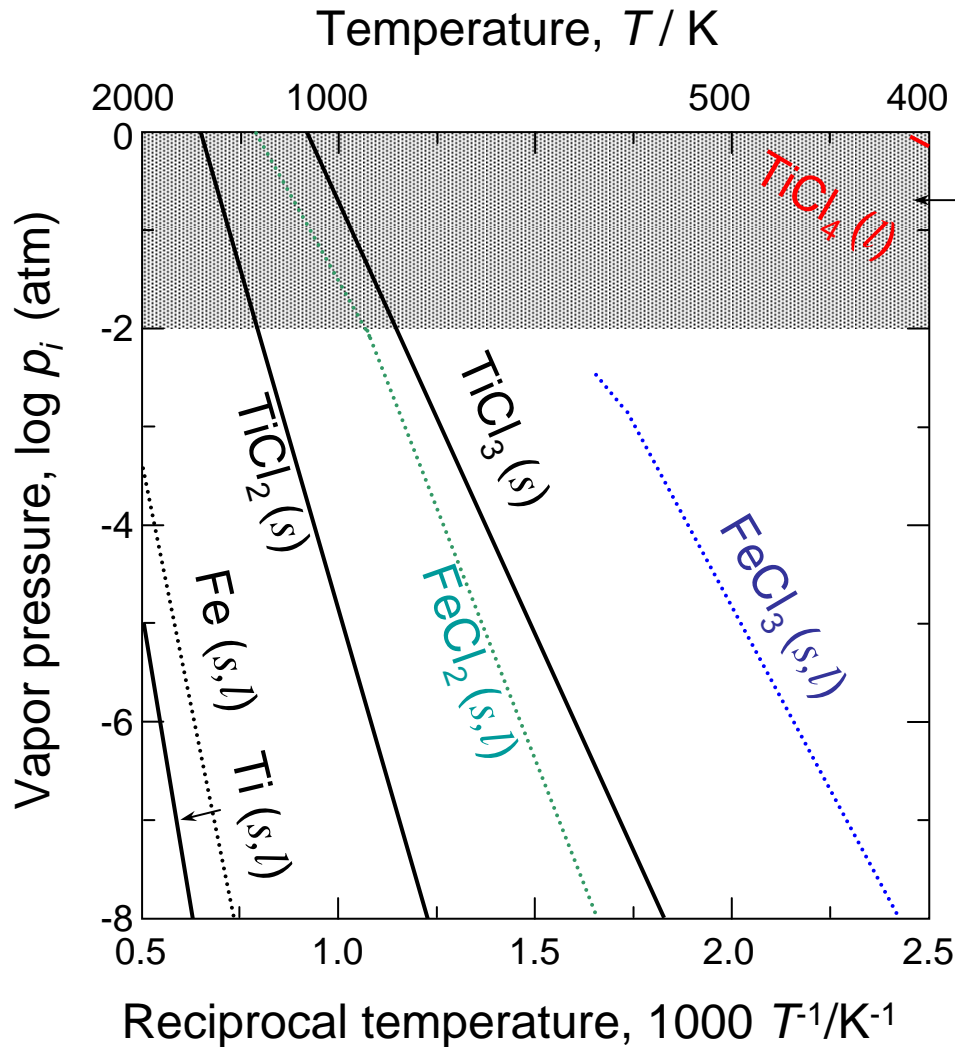


Ti present in the Ti scrap can be extracted by iron chlorides.

or

TiCl₄ can be obtained by reacting Ti scraps with chloride wastes.

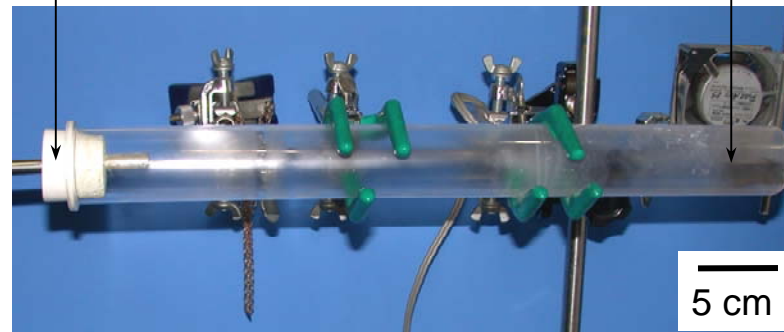
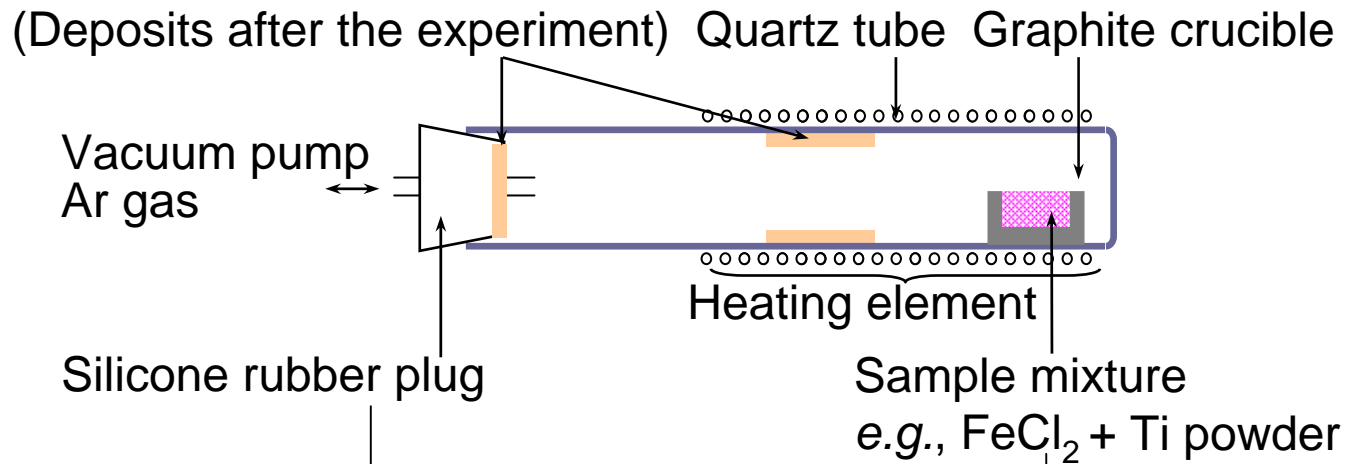
Vapor pressure of some selected chlorides and metals



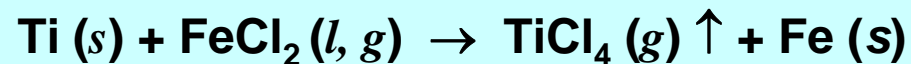
The separation of chlorides and recovery of high-purity $TiCl_4$ are possible by controlling the deposition temperature.

Vapor pressure of some chlorides and metals as a function of reciprocal temperature.

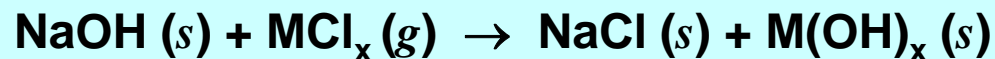
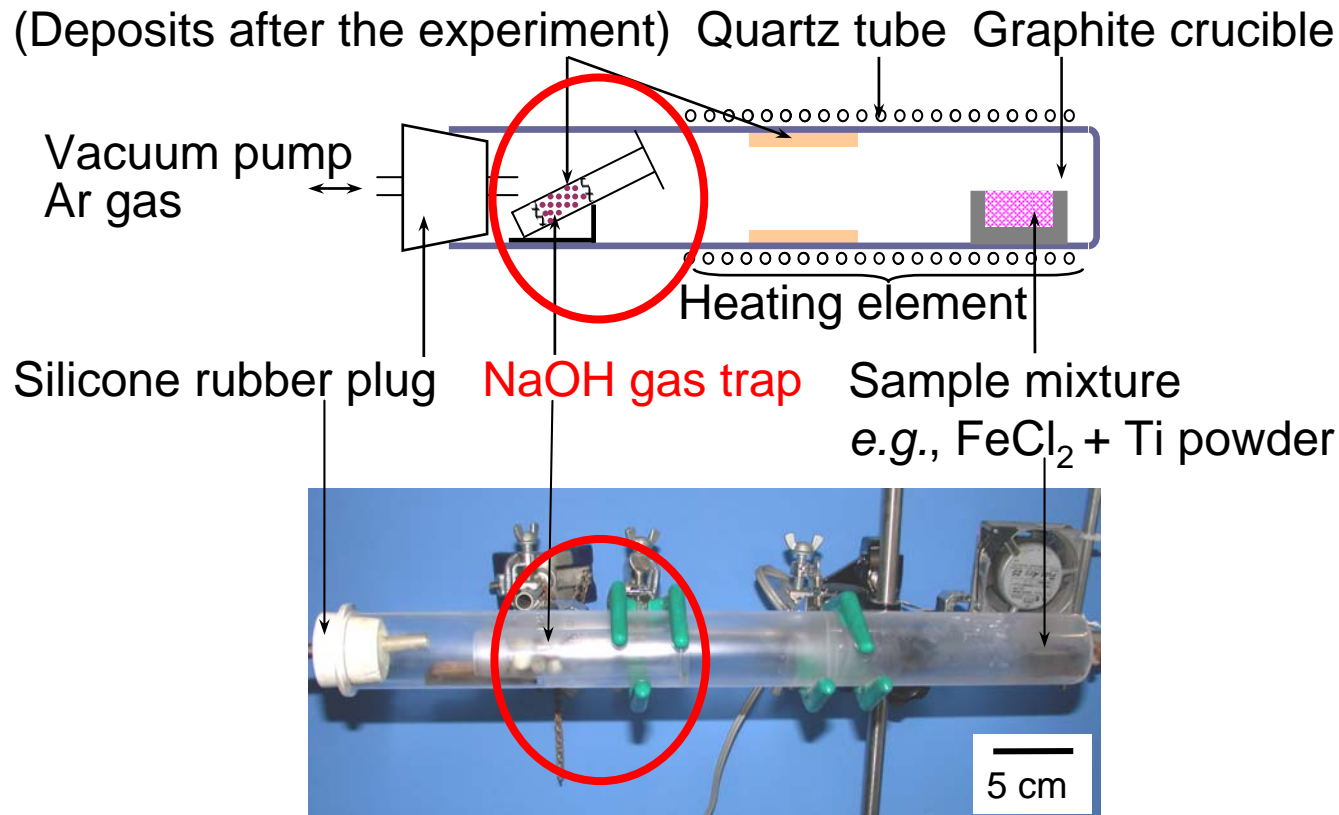
Experiment apparatus (1)



$T = 1100 \text{ K}$; $t' = 1 \text{ h}$ or 3 h ; Ar atmosphere



Experiment apparatus (2)



Experiment conditions

Exp. No.	Mass of feed materials, w_i / g			Mass Ratio w_{Ti} / w_{FeCl_2}	Reaction temp., T / K	Reaction time, t / h	Atmosphere*
	Ti scraps	FeCl ₂ (Powder)	NaOH				
CA ^a	0.33	1.90	5.27	5.79	1100	1	Ar
CB ^a	0.30	1.75	3.18	5.79	1100	1	Ar
CC ^a	0.32	1.72	-	5.36	1100	1	Ar
CD ^b	0.49	2.76	3.25	5.63	1100	3	Ar
CE ^b	0.51	2.86	5.47	5.61	1100	3	Ar
CF ^c	0.50	3.17	5.38	6.39	1100	3	Ar

a: Ti powder was used in this experiment.

b: Ti shot was used in this experiment.

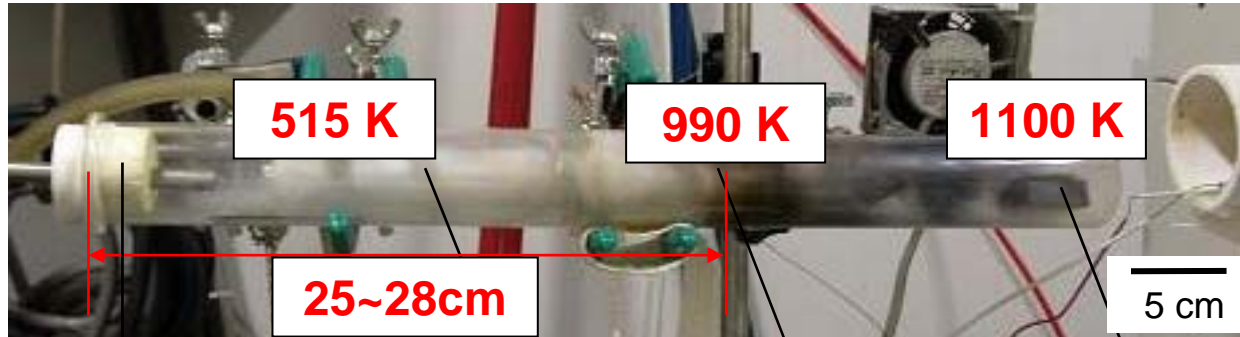
c: Ti turning was used in this experiment.

*: Reduced atmosphere (0.2 atm at room temperature).

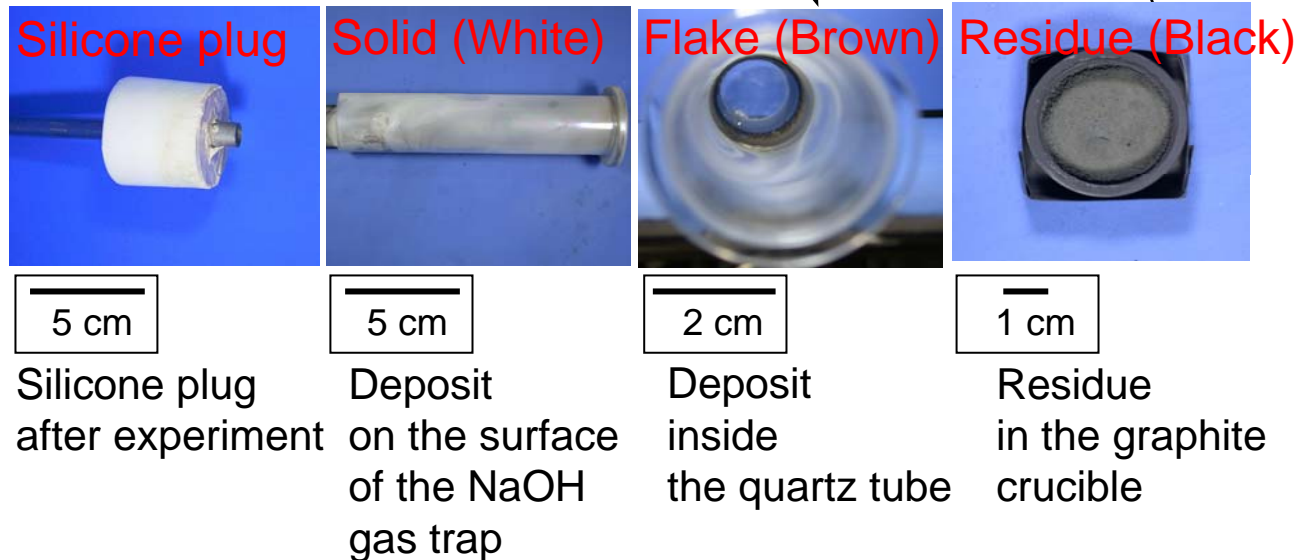
$Ti (s) + 2 FeCl_2 (l, g) = TiCl_4 (g) + 2 Fe (s)$
Stoichiometric amount of Ti to FeCl₂ is 1:5.29.

Observation

Assembled quartz tube after experiment.



The image of the obtained residue and deposit after experiment.



Melting point of FeCl_2 : 950 K @ 1 atm
 Melting point of TiCl_4 : 408 K @ 1 atm

Ti powder without NaOH gas trap: Composition

Analytical results of the samples before and after heating, and the deposits obtained on the surface of silicone plug and inside the quartz tube after heating.

Exp. CC	Concentration of element i , C_i (mass%)		
	Ti	Fe	Cl
Initial sample before heating	15.7 ^a	37.2 ^a	47.2 ^a
Residue in the graphite crucible	8.95 ^b	91.1 ^b	-
Deposit inside the quartz tube	0.33 ^c	56.2 ^c	43.4 ^c
Deposit on the surface of silicone plug	(16.7 ^b)	(2.22 ^b)	(81.1 ^d)

The value excludes carbon and gaseous elements except Cl.

a: Calculated.

b: Determined by inductively coupled plasma-atomic emission spectrometry (ICP-AES).

c: Determined by X-ray fluorescence analysis (XRF).

d: Determined by potentiometric titration method.

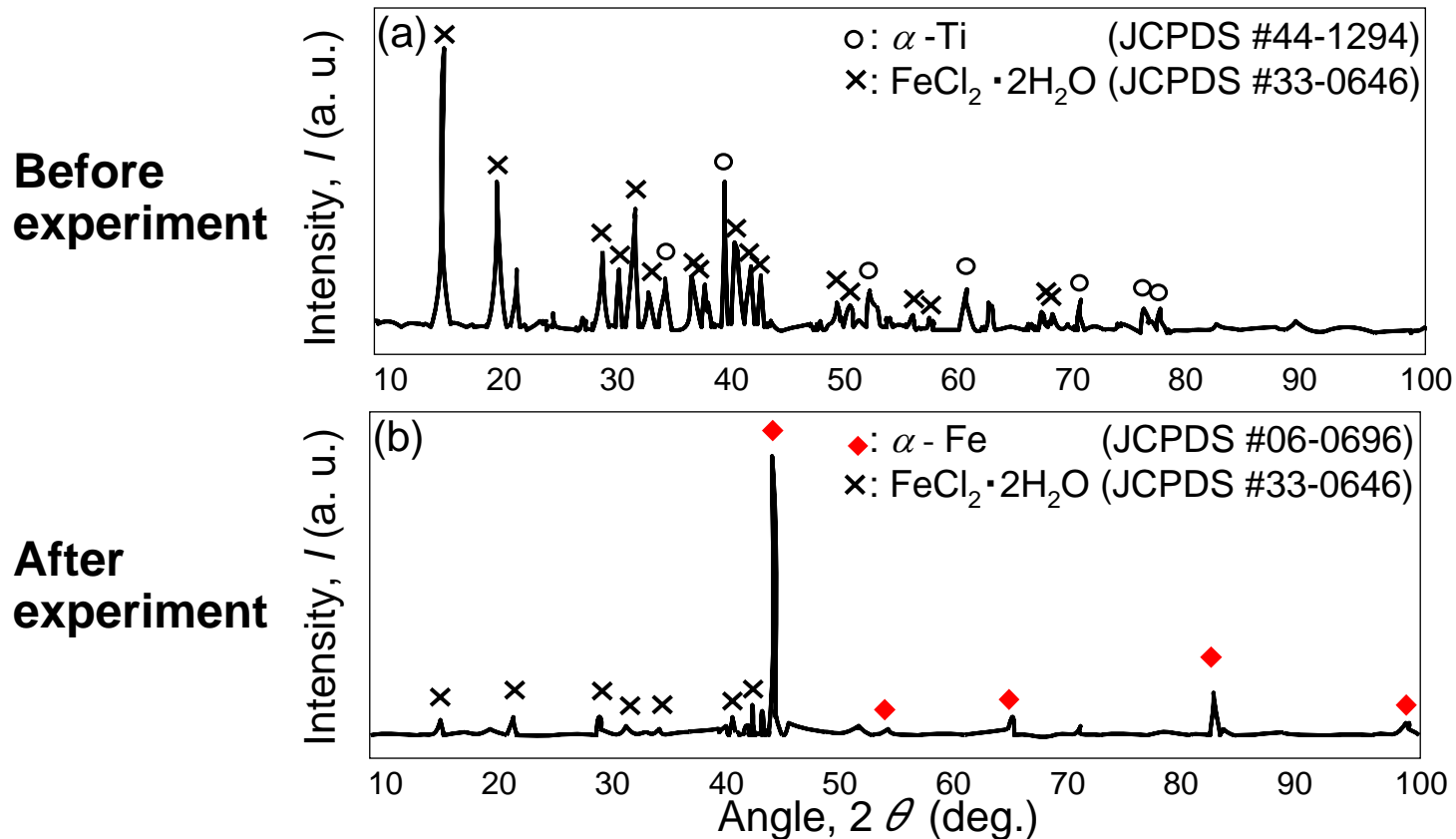
C_{Ti} : 15.7% → 8.95%.

C_{Fe} : 37.2% → 91.1%.

$TiCl_x$ ($TiCl_4$) obtained.

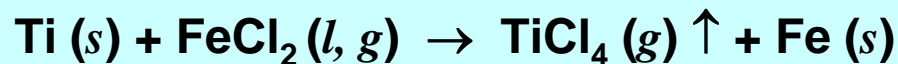
The silicone plug was damaged due to the reaction with $TiCl_4$.

Ti powder without NaOH gas trap: XRD



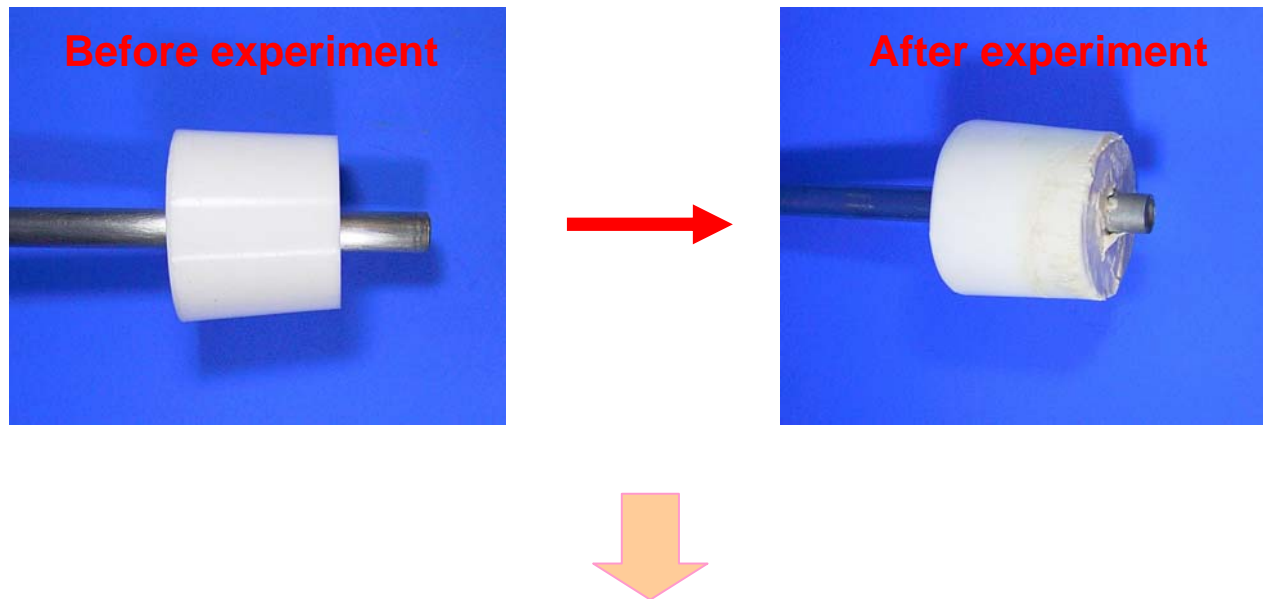
XRD patterns of the sample before experiment (a) and the residue after experiment (b) (Exp. CC)

Fe was generated at heating zone.



Discussion

Ti in Ti scraps was recovered by FeCl_2 as the form of TiCl_4 , but the silicone plug was damaged due to the reaction with the TiCl_4 .



NaOH was introduced as a gas trap for recovering TiCl_4 .

Ti powder: Composition

Analytical results of the samples before and after heating, and the deposits obtained on the surface of the NaOH gas trap and inside the quartz tube after heating.

Exp. CB	Concentration of element i , C_i (mass%) ^a		
	Ti	Fe	Cl
Initial sample before heating	14.6 ^a	37.5 ^a	47.8 ^a
Residue in the graphite crucible	4.90 ^b	95.1 ^b	-
Deposit inside the quartz tube	2.71 ^c	54.6 ^c	42.7 ^c
Deposit on the surface of the NaOH gas trap	(16.7 ^b)	(0.85 ^b)	(87.9 ^d)

The value excludes carbon and gaseous elements (except Cl).

a: Calculated.

b: Determined by inductively coupled plasma-atomic emission spectrometry (ICP-AES).

c: Determined by X-ray fluorescence analysis (XRF).

d: Determined by potentiometric titration method.

C_{Ti} : 14.6% → 4.90%.

C_{Fe} : 37.5% → 95.1%.

There was no damage on the silicone plug.

→ The obtained TiCl_4 was recovered by NaOH successfully.

Ti granule and turning: Composition

Exp. CD (Feed material: Ti granule)	Concentration of element i , C_i (mass%)		
	Ti	Fe	Cl
Initial sample before heating	15.1 ^a	37.4 ^a	47.5 ^a
Residue in the graphite crucible	62.8 ^b	37.2 ^b	-
Deposit inside the quartz tube	0.10 ^b	49.7 ^b	50.2 ^c
Deposit on the surface of NaOH gas trap	0.15 ^b	0.38 ^b	99.5 ^c

Exp. CF (Feed material: Ti turning)	Concentration of element i , C_i (mass%) ^a		
	Ti	Fe	Cl
Initial sample before heating	13.6 ^a	38.1 ^a	48.3 ^a
Residue in the graphite crucible	29.1 ^d	64.7 ^d	6.18 ^d
Deposit inside the quartz tube	0.06 ^d	50.3 ^d	49.6 ^d
Deposit on the surface of the NaOH gas trap	(0.04 ^d)	(1.29 ^d)	(98.7 ^d)

The value excludes carbon and gaseous elements (except Cl).

a: Calculated.

b: Determined by inductively coupled plasma-atomic emission spectrometry (ICP-AES).

c: Determined by the potentiometric titration method.

d: Determined by X-ray fluorescence analysis (XRF).

Black coat was formed on the surface of the residue.

The residue was magnetic material.

Fe element presents in the residue after heating.

Mass balance

Exp. #	Form of Ti scraps	Mass of feed materials, w_i / g		Mass of the obtained sample, w / g	Concentration of Ti (mass%)	Recovery Ratio of Ti, R (%)
		Ti scraps	FeCl ₂ (Powder)			
CA ^b	Powder	0.33	1.90	0.56	1.89	97
CB ^b	Powder	0.30	1.75	0.72	4.90	88
CC ^b	Powder	0.32	1.72	0.66	8.95	82
CD ^c	Granule	0.49	2.76	0.73	62.8	6.8
CE ^c	Granule	0.51	2.86	0.62	45.3	45
CF ^d	Turning	0.50	3.17	0.62	29.1	64

a: Experiment date.

b: Ti powder was used in this experiment.

c: Ti granules was used in this experiment.

d: Ti turning was used in this experiment.

When Ti powder was used as the feed material, recovery ratio of Ti was obviously higher than those when Ti granule or turning was used.

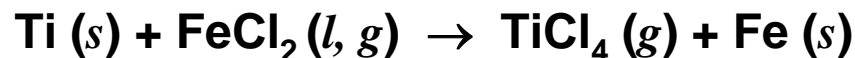


The reaction speed was affected by the morphology of the Ti scraps.

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Summary

1. Ti in Ti scraps was extracted by chloride wastes as the form of TiCl_4 .
2. Fe was generated at heating zone.
3. The obtained experimental results are in good agreement with the thermodynamic analysis:



4. The recovery ratio of Ti and Cl as well as the reaction speed were largely dependent on the morphology of the Ti scraps: Ti scraps in the form of powder is easier to be recycled by FeCl_2 than Ti granule or Ti turning.